

**AMENDMENTS TO THE CLAIMS:**

This listing of claims will replace all prior versions, and listings, of claims in the application:

**LISTING OF CLAIMS:**

1. (Currently Amended) A fiberoptic sensor for measuring at least one electric current or magnetic field, having  
 a light source (4),  
 N sensor heads ( $H_1, H_2, H_3$ ) that can be arranged in the shape of a coil around current conductors ( $C_1, C_2, C_3$ ) or along the magnetic field, N being a whole number with  $N \geq 2$ ,  
 at least one phase modulation unit (~~PME~~; ~~PME<sub>1</sub>~~, ~~PME<sub>2</sub>~~, ~~PME<sub>3</sub>~~), having at least one phase modulator (~~PM~~; ~~PM<sub>1</sub>~~, ~~PM<sub>2</sub>~~, ~~PM<sub>3</sub>~~),  
 at least one detector (~~2~~; ~~2<sub>1</sub>~~, ~~2<sub>2</sub>~~, ~~2<sub>3</sub>~~), and  
 a control and evaluation unit (5) that is connected via at least one detector signal line (~~D~~; ~~D<sub>1</sub>~~, ~~D<sub>2</sub>~~, ~~D<sub>3</sub>~~) to the at least one detector (~~2~~; ~~2<sub>1</sub>~~, ~~2<sub>2</sub>~~, ~~2<sub>3</sub>~~), and via at least one modulator signal line (~~M~~; ~~M<sub>1</sub>~~, ~~M<sub>2</sub>~~, ~~M<sub>3</sub>~~) to the at least one phase modulator (~~PM~~; ~~PM<sub>1</sub>~~, ~~PM<sub>2</sub>~~, ~~PM<sub>3</sub>~~),  
 first means (6) being provided for guiding light from the light source (4) into an end (~~3~~; ~~3<sub>1</sub>~~, ~~3<sub>2</sub>~~, ~~3<sub>3</sub>~~), on the detector side, of the phase modulation unit (~~PME~~; ~~PME<sub>1</sub>~~, ~~PME<sub>2</sub>~~, ~~PME<sub>3</sub>~~),  
 second means (7) being available for guiding light from the end (~~3~~; ~~3<sub>1</sub>~~, ~~3<sub>2</sub>~~, ~~3<sub>3</sub>~~), on the detector side, of the phase modulation unit (~~PME~~; ~~PME<sub>1</sub>~~, ~~PME<sub>2</sub>~~, ~~PME<sub>3</sub>~~) to the detector (~~2~~; ~~2<sub>1</sub>~~, ~~2<sub>2</sub>~~, ~~2<sub>3</sub>~~),  
 the at least one phase modulation unit (~~PME~~; ~~PME<sub>1</sub>~~, ~~PME<sub>2</sub>~~, ~~PME<sub>3</sub>~~) having a further end (~~4~~; ~~4<sub>1</sub>~~, ~~4<sub>2</sub>~~, ~~4<sub>3</sub>~~), on the sensor head side, that is optically connected to at least one of the sensor heads ( $H_1, H_2, H_3$ ), and

wherein by means of the at least one phase modulation unit (~~PME; PME<sub>1</sub>, PME<sub>2</sub>, PME<sub>3</sub>~~) linearly polarized lightwaves can be phase-modulated differentially in a non-reciprocal fashion, ~~characterized in that~~ wherein N modulation amplitudes  $\phi_{0,n}$  and N modulation frequencies  $\nu_n$  are provided for the non-reciprocal differential phase modulations, the modulation frequencies  $\nu_n$  and two prescribable positive whole numbers p, q with  $p \neq q$  being selected in such a way that it holds for all positive whole numbers z and for all whole numbers n, m with  $n \neq m$  and  $1 \leq n, m \leq N$  that:

$$p \cdot \nu_n \neq z \cdot \nu_m \text{ and}$$

$$q \cdot \nu_n \neq z \cdot \nu_m,$$

and the modulation amplitudes  $\phi_{0,n}$  and the modulation frequencies  $\nu_n$  being selected as a function of modulation-relevant optical path lengths  $\ell_n$ .

2. (Currently Amended) The sensor as claimed in claim 1, ~~characterized in that~~ wherein exactly one control and evaluation unit (5) is provided, in which signals that originate from the various sensor heads (~~H<sub>1</sub>, H<sub>2</sub>, H<sub>3</sub>~~) and are fed to the control and evaluation unit (5) via the at least one detector signal line (~~D<sub>1</sub>, D<sub>2</sub>, D<sub>3</sub>~~) can be distinguished from one another by means of frequency filtering, it being possible to convert these signals into N output signals  $S_n$ , in particular it being possible to determine the output signals  $S_n$  for each n with  $1 \leq n \leq N$  from signals at the frequencies  $p \cdot \nu_n$  and  $q \cdot \nu_n$  in the control and evaluation unit (5).

3. (Currently Amended) The sensor as claimed in ~~one of claims 1 or 2~~ claim 1, ~~characterized in that~~ wherein exactly one phase modulation unit (~~PME~~) is provided, and in that N reflection interferometers are provided, each of the N reflection interferometers

including exactly one of the N sensor heads ( $H_1, H_2, H_3$ ), and the N sensor heads ( $H_1, H_2, H_3$ ) in each case having a mirrored end ( $13_1, 13_2, 13_3$ ).

4. (Currently Amended) The sensor as claimed in claim 3, ~~characterized in that~~ wherein the light source (4) is connected to the control and evaluation unit (5) via a light control signal line (L), and in that a time division multiplexing method is provided for the measurement.

5. (Currently Amended) The sensor as claimed in ~~one of claims 3 or 4~~ claim 3, ~~characterized in that~~ wherein the phase modulation unit (PME) either  
(a) is a modulator circuit (PME) having N phase modulators ( $PM_1, PM_2, PM_3$ ), in particular piezoelectric phase modulators ( $PM_1, PM_2, PM_3$ ), each of the N phase modulators ( $PM_1, PM_2, PM_3$ ) being assigned to exactly one of the N modulation frequencies  $\nu_n$ , and ~~in that~~ wherein each of the N phase modulators ( $PM_1, PM_2, PM_3$ ) can be operated at the modulation frequency  $\nu_n$  assigned to it, and ~~in that~~ wherein the differential phase of oppositely directed lightwaves polarized parallel to one another can be modulated, or  
(b) includes a single phase modulator (PM), ~~in particular~~ configured as an integrated optical phase modulator (PM), which permits a simultaneous phase modulation with the N various modulation frequencies  $\nu_n$ , and it being possible to modulate the differential phase of lightwaves that propagate in the same direction and are mutually orthogonally polarized.

6. (Currently Amended) The sensor as claimed in ~~one of claims 1 or 2~~ claim 1, ~~characterized in that~~ wherein N phase modulation units ( $PME_1, PME_2, PME_3$ ) having one phase modulator ( $PM_1, PM_2, PM_3$ ) each are provided, the nth phase modulation unit ( $PME_n$ ) being optically connected to the nth sensor head ( $H_n$ ), and it being possible to operate the nth phase modulator ( $PM_n$ ) with the modulation frequency  $\nu_n$ , and each of the phase

modulators (~~PM<sub>1</sub>, PM<sub>2</sub>, PM<sub>3</sub>~~) being connected to the control and evaluation unit (5) via one modulator signal line (~~M<sub>1</sub>, M<sub>2</sub>, M<sub>3</sub>~~) each.

7. (Currently Amended) The sensor as claimed in claim 6, ~~characterized in that~~ wherein N reflection interferometers are provided, each of the N reflection interferometers comprising exactly one of the N sensor heads (~~H<sub>1</sub>, H<sub>2</sub>, H<sub>3</sub>~~), and the N sensor heads (~~H<sub>1</sub>, H<sub>2</sub>, H<sub>3</sub>~~) in each case having a mirrored end (~~13<sub>1</sub>, 13<sub>2</sub>, 13<sub>3</sub>~~), and

~~in that~~ wherein either

(a) the phase modulation units (~~PME<sub>1</sub>, PME<sub>2</sub>, PME<sub>3</sub>~~) are modulator circuits (~~PME<sub>1</sub>, PME<sub>2</sub>, PME<sub>3</sub>~~), and ~~in that~~ wherein it is possible to modulate the differential phase of oppositely directed lightwaves polarized parallel to one another by means of the phase modulators (~~PM<sub>1</sub>, PM<sub>2</sub>, PM<sub>3</sub>~~), and ~~in particular in that~~ wherein the phase modulators

(~~PM<sub>1</sub>, PM<sub>2</sub>, PM<sub>3</sub>~~) are piezoelectric phase modulators (~~PM<sub>1</sub>, PM<sub>2</sub>, PM<sub>3</sub>~~), or

(b) each of the phase modulators (~~PM<sub>1</sub>, PM<sub>2</sub>, PM<sub>3</sub>~~) can modulate the differential phase of mutually orthogonally polarized lightwaves propagating in the same direction and, ~~in particular, in that~~ wherein the phase modulators (~~PM<sub>1</sub>, PM<sub>2</sub>, PM<sub>3</sub>~~) are integrated optical phase modulators (~~PM<sub>1</sub>, PM<sub>2</sub>, PM<sub>3</sub>~~).

8. (Currently Amended) The sensor as claimed in claim 6, ~~characterized in that~~ wherein N Sagnac interferometers are provided, each of the N Sagnac interferometers including exactly one of the N sensor heads (~~H<sub>1</sub>, H<sub>2</sub>, H<sub>3</sub>~~), and ~~in that~~ wherein each of the phase modulation units (~~PME<sub>1</sub>, PME<sub>2</sub>, PME<sub>3</sub>~~) is essentially one phase modulator (~~PM<sub>1</sub>, PM<sub>2</sub>, PM<sub>3</sub>~~) each, it being possible to modulate the differential phase of oppositely directed lightwaves, polarized parallel to one another, by means of the phase modulators (~~PM<sub>1</sub>, PM<sub>2</sub>, PM<sub>3</sub>~~), and ~~in particular, in that~~ wherein the phase modulators (~~PM<sub>1</sub>, PM<sub>2</sub>, PM<sub>3</sub>~~) are piezoelectric phase modulators (~~PM<sub>1</sub>, PM<sub>2</sub>, PM<sub>3</sub>~~) or integrated optical modulators (~~PM<sub>1</sub>, PM<sub>2</sub>, PM<sub>3</sub>~~).

9. (Currently Amended) The sensor as claimed in ~~one of the preceding claims~~ claim 1, characterized in that wherein selection  $p = 1$  and  $q = 2$  is made, and in that the  $N$  modulation amplitudes  $\phi_{0,n}$  and the  $N$  modulation frequencies  $\nu_n$  are selected in such a way that amplitudes  $\alpha_{0,n}$  of the modulation of the differential phase of the linearly polarized lightwaves lie between 1.7 and 2.0, in particular between 1.8 and 1.88, or are essentially 1.84 for all  $n$  with  $1 \leq n \leq N$ .

10. (Currently Amended) The sensor as claimed in ~~one of the preceding claims~~ claim 1, characterized in that wherein either  
 (a) exactly one detector ~~(2)~~ is provided, or  
 (b)  $N$  detectors ~~(2<sub>1</sub>, 2<sub>2</sub>, 2<sub>3</sub>)~~ are provided, each of the detectors ~~(2<sub>1</sub>, 2<sub>2</sub>, 2<sub>3</sub>)~~ being connected to the control and evaluation unit ~~(5)~~ via one detector signal line ~~(D<sub>1</sub>, D<sub>2</sub>, D<sub>3</sub>)~~ each.

11. (Currently Amended) The sensor as claimed in ~~one of the preceding claims~~ claim 1, characterized in that wherein  $N = 3$  or  $N = 6$ , and the electric currents of three phases of an electric high voltage system can be measured by means of one sensor head ~~(H<sub>1</sub>, H<sub>2</sub>, H<sub>3</sub>)~~ each in the case of  $N = 3$ , or being able to be measured by means of two sensor heads ~~(H<sub>1</sub>)~~ each in the case of  $N = 6$ .

12. (Currently Amended) A method for measuring at least one electric current or at least one magnetic field, a light source ~~(1)~~ emitting lightwaves that are converted into linearly polarized lightwaves, and  
 the linearly polarized lightwaves being guided into  $N$  sensor heads ~~(H<sub>1</sub>, H<sub>2</sub>, H<sub>3</sub>)~~ in which the lightwaves undergo a phase shift, which phase shift depends on the current or magnetic field to be measured,  $N$  being a whole number with  $N \geq 2$ , and

the lightwaves being detected in at least one detector  $\{2; 2_1, 2_2, 2_3\}$ , and  
the lightwaves undergoing a non-reciprocal differential phase modulation in at least one  
phase modulation unit  $\{PME; PME_1, PME_2, PME_3\}$  having at least one phase modulator  
 $\{PM; PM_1, PM_2, PM_3\}$ , the at least one phase modulation unit  $\{PME; PME_1, PME_2, PME_3\}$  being  
traversed by the lightwaves both during their propagation from the light source (4) to the  
sensor heads  $\{H_1, H_2, H_3\}$  and during their propagation from the sensor heads  $\{H_1, H_2, H_3\}$  to  
the at least one detector  $\{2; 2_1, 2_2, 2_3\}$ , and  
a control and evaluation unit (5) being used both to control the at least one phase modulator  
 $\{PM; PM_1, PM_2, PM_3\}$  and to evaluate signals originating from the at least one detector  
 $\{2; 2_1, 2_2, 2_3\}$ ,

characterized in that wherein

the lightwaves are differentially phase-modulated in a non-reciprocal fashion with N  
modulation amplitudes  $\phi_{0,n}$  and N modulation frequencies  $\nu_n$ , the modulation frequencies  $\nu_n$   
and two prescribable positive whole numbers p, q with  $p \neq q$  being selected in such a way  
that it holds for all positive whole numbers z and for all whole numbers n, m with  $n \neq m$  and  $1$   
 $\leq n, m \leq N$  that:

$$p \cdot \nu_n \neq z \cdot \nu_m \text{ and}$$

$$q \cdot \nu_n \neq z \cdot \nu_m,$$

and the modulation amplitudes  $\phi_{0,n}$  and the modulation frequencies  $\nu_n$  being selected as a  
function of modulation-relevant optical path lengths  $\ell_n$ .